

(35)

Another important point to be observed is that the set: for u & v as obtained above are valid for $\frac{U_\infty x}{\nu} \gg 1$. In the neighbourhood of the leading edge at $x=0$, the B.L. approximation fails and consequently the set: _(soln) are not valid therefore the important improved approximations are necessary [L. Roeselard].

skin friction:

The frictional force per unit area of the plate at distance x from the leading edge is called shearing stress at the wall.

In the case of flow past a flat plate

$$\sigma_w = \left(\sigma_{xy} \right)_{y=0} = \mu \left(\frac{\partial u}{\partial y} \right)_{y=0} = \mu U_\infty f''(0) \sqrt{\frac{U_\infty}{\nu x}}$$

$$\sigma_w = \mu U_\infty \alpha \sqrt{\frac{U_\infty}{\nu x}}, \text{ where } \alpha = f''(0) = 0.332$$

$$= \rho \nu U_\infty \alpha \frac{1}{\sqrt{\frac{\nu x}{U_\infty} + \frac{U_\infty^2}{\nu^2}}} \propto \frac{U_\infty}{\sqrt{x}}$$

$$= \rho U_\infty \alpha \frac{1}{\sqrt{\frac{U_\infty x}{\nu}}} = \rho U_\infty (0.332) \frac{1}{\sqrt{R_L}}, \text{ where } R_L \text{ is the Reynolds no.}$$

Hence the dimensionless shearing stress which is also known as local skin friction coefficient is given by

$$C_f = \frac{\sigma_w}{\rho U_\infty^2 / 2} = \frac{0.664}{\sqrt{R_L}}$$

The drag extend on the two sides of a plate of length l width b is given by

$$D = 2b \int_0^l \left(\sigma_{xy} \right)_{y=0} dx$$

$$\begin{aligned}
 &= 4d b \rho (U_\infty^3 l \nu)^{1/2} \\
 &= 1.328 b \rho (R_L \nu U_\infty^2)^{1/2} \\
 &= 1.328 b \rho R_L^{1/2} \nu^{1/2} U_\infty
 \end{aligned}$$

Hence a dimensionless drag coefficient

$$C_D = \frac{\text{Drag}}{\frac{1}{2} \rho A U_\infty^2}, \quad \text{where } A = 2bl \text{ denotes the total wetted surface area.}$$

Hence,

$$\begin{aligned}
 C_D &= \frac{1.328 b \rho R_L^{1/2} \nu^{1/2} U_\infty}{\frac{1}{2} \rho \cdot 2bl U_\infty^2} \\
 &= \frac{1.328 R_L^{1/2}}{R_L} \\
 &= 1.328 R_L^{-1/2}
 \end{aligned}$$

Note: The similarity solution is also called the exact solution of b.l. equation.

§: Blasius solution:

The problem of the B.L. flow along a thin flat plate at zero incidence in a uniform stream was first discovered by Blasius (1908).

Blasius solution of the B.L. equation:

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = U_\infty \frac{\partial U_\infty}{\partial x} + \nu \frac{\partial^2 u}{\partial y^2} \quad \rightarrow (1)$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \quad \rightarrow (2)$$

subject to the boundary condition

$$\left. \begin{aligned} u = v = 0 & \text{ at } y = 0 \\ u = U_{\infty} & \text{ at } y \rightarrow \infty \end{aligned} \right\} \rightarrow (3)$$

do not differ in sense from the similarity solution. The equation (2) can be integrated by introducing a stream function $\psi(x, y)$ s.t.

$$u = -\frac{\partial \psi}{\partial y}, \quad v = \frac{\partial \psi}{\partial x}$$

Blasius solution: for the stream function is of the form

$$\psi = \sqrt{U_{\infty} \nu x} f(\eta)$$

where f is non-dimensional function. In the variable η is defined by $\eta = \sqrt{\frac{U_{\infty}}{\nu x}} y$

Blasius took the principle of similarity for velocity profile in the B.L. as

$$\frac{U}{U_{\infty}} = \phi\left(\frac{y}{\delta}\right), \text{ where } \delta(x) \sim \sqrt{\frac{\nu x}{U_{\infty}}}$$

Now, substituting the values of $u, v, \frac{\partial u}{\partial x}, \frac{\partial v}{\partial y}, \frac{\partial^2 u}{\partial y^2}$ etc. in (1) we get the differential equation.

$$ff'' + 2f''' = 0 \rightarrow (4) \text{ (Usually known as Blasius equation)}$$

subject to boundary condition

$$\left. \begin{aligned} f = f' = 0 & \text{ at } \eta = 0 \\ f' = 1 & \text{ at } \eta \rightarrow \infty \end{aligned} \right\} \rightarrow (5)$$

Blasius obtained the set of (4) in the form of a series expansion for η small and an analytic expansion for η large, the two forms being matched at a suitable value of η .

Series solution for η small:

Since $f=f'=0$ at $\eta=0$, a series for $f(\eta)$ is

$$f(\eta) = c_2 \frac{\eta^2}{L^2} + c_3 \frac{\eta^3}{L^3} + c_4 \frac{\eta^4}{L^4} + c_5 \frac{\eta^5}{L^5} + \dots + c_n \frac{\eta^n}{L^n} + \dots$$

$$f'(\eta) = c_2 \eta + c_3 \frac{\eta^2}{L^2} + c_4 \frac{\eta^3}{L^3} + c_5 \frac{\eta^4}{L^4} + \dots$$

$$f''(\eta) = c_2 + c_3 \eta + c_4 \frac{\eta^2}{L^2} + c_5 \frac{\eta^3}{L^3} + \dots$$

$$f'''(\eta) = c_3 + c_4 \eta + c_5 \frac{\eta^2}{L^2} + \dots$$

Substituting these in the Blasius equation, we get,

$$0 = 2c_3 + 2c_4\eta + (c_2^2 + 2c_5) \frac{\eta^2}{L^2} + (2c_6 + 4c_2c_3) \frac{\eta^3}{L^3} + \dots$$

Now, comparing the coefficients of different powers of η on both sides, we get,

$$c_3 = 0, c_4 = 0, c_5 = -\frac{1}{2} c_2^2, c_6 = 0, c_7 = 0, c_8 = -\frac{11}{21} c_2 c_5$$

All the non-zero coefficients are found to depend only on c_2 .

Now, obviously, $c_2 = f''(0) = \alpha$ (say)

For small η ,

$$f(\eta) = c_2 \frac{\eta^2}{L^2} + c_3 \frac{\eta^3}{L^3} + c_4 \frac{\eta^4}{L^4} + \dots$$

$$= \frac{\eta^2}{1 \cdot L^2} \alpha - \frac{\eta^5}{2 \cdot L^5} \frac{\alpha^2}{L^2} + \frac{\eta^8}{2^2 \cdot L^8} \frac{11 \cdot \alpha^3}{L^3} - \dots$$